

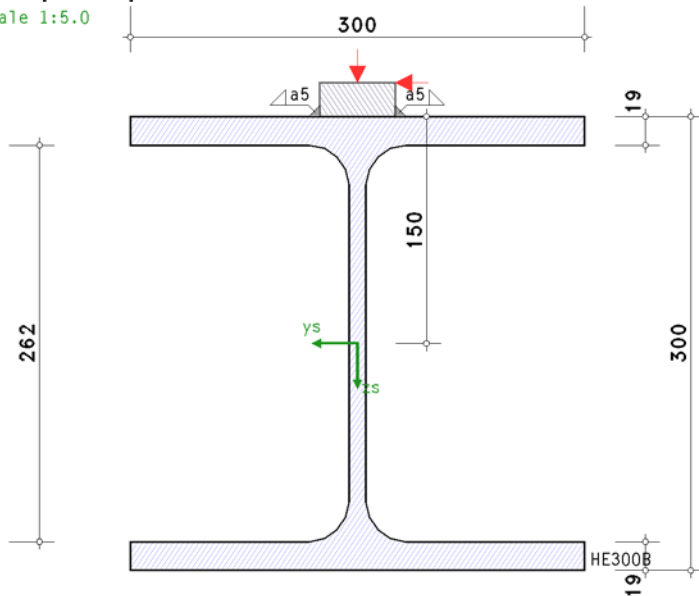
POS. 4: BSP. 2 WHEEL PRESSURE TOP FLANGE

detailed problems acc. to Eurocode 3, EC 3-6 (12.10), NA: Deutschland

4H-EC3LK version: 11/2016-1f

1. input report

scale 1:5.0



steel grade

steel grade S235

cross-section

beam: section HE300B

crane gantry

crane rail of flat steel, shear-resistant joined with the girder

connection with fillet welds: weld thickness $a_w = 5.0$ mm (continuous)

crane rail: width $b_r = 50.0$ mm, height $h = 30.0$ mm, 25% wear

height, cross-sectional area, moments of inertia of fretted rail $h_r = 22.5$ mm, $A_r = 11.25$ cm²,

$I_{yr} = 4.75$ cm⁴, $I_{tr} = 14.18$ cm⁴

loading

internal forces and moments at limit state of resistance (ULS):

Lk 1: $M_{y,Ed} = 100.0$ kNm, $V_{z,Ed} = 130.0$ kN

internal forces and moments at limit state of serviceability (SLS):

Lk 1: $M_{y,Ed} = 129.8$ kNm, $V_{z,Ed} = 175.5$ kN

transverse loading on upper edge of cross-section:

vertical wheel pressure $F_{z,Ed,ULS} = 100.00$ kN, $F_{z,Ed,SLS} = 113.70$ kN

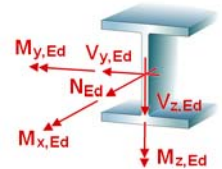
horizontal wheel pressure $H_{Ed,SLS} = 17.40$ kN, $H_{Ed,ULS} = 15.00$ kN

partial safety factors for material

resistance of cross-sections $\gamma_{M0} = 1.00$

resistance of bolts, welds, plates in bearing $\gamma_{M2} = 1.25$

serviceability $\gamma_{M,ser} = 1.00$



2. verification der local loading due to crane gantry

cross-sectional properties: $A = 149.08$ cm², $z_s = 150.0$ mm, $I_y = 25165.90$ cm⁴, $y_s = 0.0$ mm, $I_z = 8562.83$ cm⁴

effective loading length from crane gantry:

$l_{eff} = 3.25 \cdot (I_{tr}/t_w)^{1/3} = 107.1$ mm

length of local loading:

referring to outer edge of flange $s_s = l_{eff} - 2 \cdot t_f = 69.1$ mm / auf den webanschnitt $s_w = l_{eff} + 2 \cdot r = 161.1$ mm

2.1. compression of web (ULS)

permissible stresses: $\sigma_{Rd} = f_y/\gamma_{M0} = 235.0$ N/mm², $\tau_{Rd} = f_y/(3^{1/2} \cdot \gamma_{M0}) = 135.7$ N/mm²

wheel pressure at first cut of web:

local stresses $\sigma_{\sigma z,Ed} = -56.4$ N/mm², $\tau_{\sigma x z,Ed} = -11.3$ N/mm²

$|\sigma_{\sigma z,Ed}| = 56.4$ N/mm² < $\sigma_{Rd} = 235.0$ N/mm² $\Rightarrow U = 0.240 < 1$ ok

$|\tau_{\sigma x z,Ed}| = 11.3$ N/mm² < $\tau_{Rd} = 135.7$ N/mm² $\Rightarrow U = 0.083 < 1$ ok

stresses at first cut of web:

Lk 1: $M_{y,Ed} = 100.0 \text{ kNm}$, $V_{z,Ed} = 130.0 \text{ kN}$

stresses $\sigma_{x,Ed} = -56.4 \text{ N/mm}^2$, $\tau_{xz,Ed} = -11.3 \text{ N/mm}^2$

$|\sigma_{x,Ed}| = 56.4 \text{ N/mm}^2 < \sigma_{Rd} = 235.0 \text{ N/mm}^2 \Rightarrow U = 0.239 < 1 \text{ ok}$

$|\tau_{xz,Ed}| + |\tau_{oxz,Ed}| = 11.3 \text{ N/mm}^2 < \tau_{Rd} = 135.7 \text{ N/mm}^2 \Rightarrow U = 0.083 < 1 \text{ ok}$

$\sigma_v = 84.0 \text{ N/mm}^2 < \sigma_{Rd} = 235.0 \text{ N/mm}^2 \Rightarrow U = 0.357 < 1 \text{ ok}$

maximum utilization: $\max U_{ULS} = 0.357 < 1 \text{ ok}$

2.2. elastic behaviour (SLS)

permissible stresses: $\sigma_{Rd} = f_y/\gamma_{M,ser} = 235.0 \text{ N/mm}^2$, $\tau_{Rd} = f_y/(3^{1/2} \cdot \gamma_{M,ser}) = 135.7 \text{ N/mm}^2$

wheel pressure at top edge of the web:

local stresses $\sigma_{oz,Ed} = -64.2 \text{ N/mm}^2$, $\tau_{oxz,Ed} = -12.8 \text{ N/mm}^2$

$|\sigma_{oz,Ed}| = 64.2 \text{ N/mm}^2 < \sigma_{Rd} = 235.0 \text{ N/mm}^2 \Rightarrow U = 0.273 < 1 \text{ ok}$

$|\tau_{oxz,Ed}| = 12.8 \text{ N/mm}^2 < \tau_{Rd} = 135.7 \text{ N/mm}^2 \Rightarrow U = 0.095 < 1 \text{ ok}$

stresses at top edge of the web:

Lk 1: $M_{y,Ed} = 129.8 \text{ kNm}$, $V_{z,Ed} = 175.5 \text{ kN}$

stresses $\sigma_{x,Ed} = -64.2 \text{ N/mm}^2$, $\tau_{xz,Ed} = -12.8 \text{ N/mm}^2$

$|\sigma_{x,Ed}| = 64.2 \text{ N/mm}^2 < \sigma_{Rd} = 235.0 \text{ N/mm}^2 \Rightarrow U = 0.273 < 1 \text{ ok}$

$|\tau_{xz,Ed}| + |\tau_{oxz,Ed}| = 12.8 \text{ N/mm}^2 < \tau_{Rd} = 135.7 \text{ N/mm}^2 \Rightarrow U = 0.095 < 1 \text{ ok}$

$\sigma_v = 104.9 \text{ N/mm}^2 < \sigma_{Rd} = 235.0 \text{ N/mm}^2 \Rightarrow U = 0.446 < 1 \text{ ok}$

maximum utilization: $\max U_{SLS} = 0.446 < 1 \text{ ok}$

2.3. welds of crane rail at outer edge of flange

$N_{Ed} = -F_{z,Ed}/2 = -50.0 \text{ kN}$, $V_{Ed} = -H_{Ed}/2 = -7.5 \text{ kN}$

effective weld length $l_{eff} = l_w = 69.1 \text{ mm}$

$\sigma_{1,w,Ed} = 19.11 \text{ kN/cm}^2 < f_{1w,d} = 36.00 \text{ kN/cm}^2 \Rightarrow U = 0.531 < 1 \text{ ok}$

$\sigma_{2,w,Ed} = 11.77 \text{ kN/cm}^2 < f_{2w,d} = 25.92 \text{ kN/cm}^2 \Rightarrow U = 0.454 < 1 \text{ ok}$

$N_{Ed} = -50.0 \text{ kN}$, $V_{Ed} = H_{Ed}/2 = 7.5 \text{ kN}$

effective weld length $l_{eff} = l_w = 69.1 \text{ mm}$

$\sigma_{1,w,Ed} = 19.11 \text{ kN/cm}^2 < f_{1w,d} = 36.00 \text{ kN/cm}^2 \Rightarrow U = 0.531 < 1 \text{ ok}$

$\sigma_{2,w,Ed} = 11.77 \text{ kN/cm}^2 < f_{2w,d} = 25.92 \text{ kN/cm}^2 \Rightarrow U = 0.454 < 1 \text{ ok}$

3. final result

maximum utilization: $\max U = 0.531 < 1 \text{ ok}$

verification succeeded

4. Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-1/A1, Ergänzungen zur DIN EN 1993-1-1, Ausgabe Juli 2014

DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe September 2017

DIN EN 1993-6, Eurocode 3: Bemessung und Konstruktion von Stahlbauten - Teil 6: Kranbahnen;

Deutsche Fassung EN 1993-6:2007 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-6/NA, Nationaler Anhang zur DIN EN 1993-6, Ausgabe Dezember 2010