

POS. 10: TYPED IG-CONNECTION

standard IG-connection

hinged IG-connection acc. to EC 3-1-8 (12.10), NA: Deutschland

the connection type, dimensions of beam, bolts, end-plate resp. angle and material are taken of the following literature:

'Typisierte Anschlüsse im Stahlhochbau nach DIN EN 1993-1-8, Stahlbau Verlags- und Service GmbH, Ausgabe 2013' the current number and associated parameters are recorded. verification method is 'elastic-elastic'. bolts are not preloaded.

code IG, steel grade S 235, bolt class of bolts 4.6

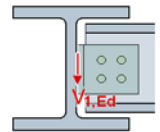
160: beam section IPE400, connection type 1, bolt size M24, 3 bolt-rows

angle: L200x100x12, $h_{wi} = 260$ mm

$e_{z,mg} = 50$ mm, $p_{z,mg} = 80$ mm, $e_{x,mg} = 50$ mm, $e_{z,sb} = 50$ mm, $p_{z,sb} = 80$ mm, $e_{x,sb} = 50$ mm

$V_{j,Ed}$: internal forces and moments at hinge

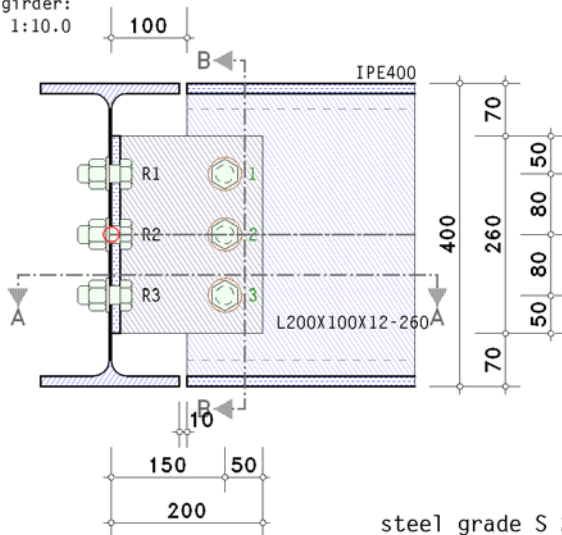
Lk	$V_{j,Ed}$ kN		Lk	$V_{j,Ed}$ kN		Lk	$V_{j,Ed}$ kN	
--			--			--		
1	27.22	min N	5	-6.85	min V_{ζ}	9	-22.74	min V_{η}
2	89.08	max N	6	63.25	min σ_l	10	-79.40	min V_{ζ}
3	26.19	min V_{η}	7	-68.00	min N	11	-4.22	max V_{ζ}
4	89.70	max V_{η}	8	-23.21	max N			



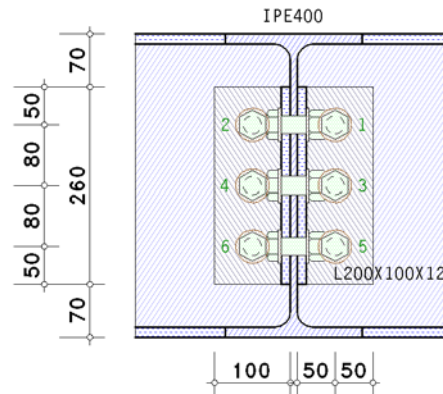
Simple Joint of Beams

EC 3-1-8 (12.10), NA: Deutschland

main girder:
scale 1:10.0



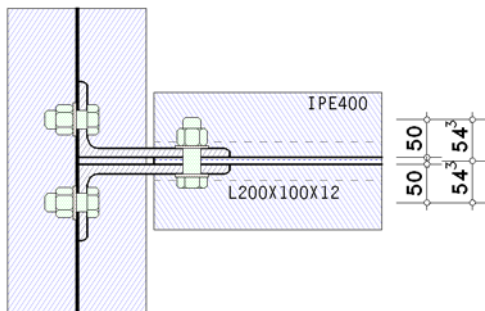
section B-B:



steel grade S 235
bolts M24-4.6

○ hinge

section A-A:



partial safety factors for material

resistance of cross sections $\gamma_{M0} = 1.00$

resistance of bolts, welds, plates in bearing $\gamma_{M2} = 1.25$

resistance with tension loads $\gamma_{Mu} = 1.10$

Final Result

maximum utilization [Lk 4]: design resistance max $U = 0.847 < 1$ **ok.**

verification succeeded

Decisive load case combination

notes

design resistance of the main girder is not verified.

distances between bolts are not checked.

Lk 4: max V_{η}

design values

transformation of member forces to the reference point (intersection point of beam axis')

$$M_{1,Ed} = V_{j1,Ed} \cdot e_1 = -0.13 \text{ kNm}, \quad e_1 = -1.5 \text{ mm}$$

$$V_{1,Ed} = V_{j1,Ed} = 89.70 \text{ kN}$$

design resistance of the connection

angle leg at main girder:

shear force resistance

bolts in shear:

$$\text{design shear resistance per shear plane: } F_{v,Rd} = \alpha_v \cdot f_{ub} \cdot A / \gamma_{M2} = 86.86 \text{ kN}, \quad \alpha_v = 0.60$$

$$\text{design shear resistance total: } V_{Rd,1} = 334.3 \text{ kN}$$

angle leg 2 with bearing resistance:

$$\text{design bearing resistance total: } V_{Rd,2} = 581.8 \text{ kN}$$

angle leg 2 with shear (gross section):

$$\text{shear resistance } V_{Rd} = (A_v \cdot f_y) / (3^{1/2} \cdot \gamma_{M0}) = 423.31 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,3} = 2 \cdot V_{Rd} / 1.27 = 666.6 \text{ kN}$$

angle leg 2 with shear (net section):

$$\text{shear resistance } V_{Rd} = (A_{v,net} \cdot f_u) / (3^{1/2} \cdot \gamma_{M2}) = 363.15 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,4} = 2 \cdot V_{Rd} = 726.3 \text{ kN}$$

$$\text{shear resistance: } \min V_{Rd,a2} = V_{Rd,1} = 334.3 \text{ kN}$$

angle leg at supported beam:

shear force resistance

bolts in shear:

$$\text{design shear resistance per shear plane: } F_{v,Rd} = \alpha_v \cdot f_{ub} \cdot A / \gamma_{M2} = 86.86 \text{ kN}, \quad \alpha_v = 0.60$$

$$\text{design shear resistance total: } V_{Rd,1} = 174.6 \text{ kN}$$

angle leg 1 with bearing resistance:

$$\text{design bearing resistance total: } V_{Rd,2} = 795.9 \text{ kN}$$

angle leg 1 with shear (gross section):

$$\text{shear resistance } V_{Rd} = (A_v \cdot f_y) / (3^{1/2} \cdot \gamma_{M0}) = 423.31 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,3} = 2 \cdot V_{Rd} / 1.27 = 666.6 \text{ kN}$$

angle leg 1 with shear (net section):

$$\text{shear resistance } V_{Rd} = (A_{v,net} \cdot f_u) / (3^{1/2} \cdot \gamma_{M2}) = 363.15 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,4} = 2 \cdot V_{Rd} = 726.3 \text{ kN}$$

angle leg 1 in tension and shear (shear block):

$$\text{shear resistance } V_{eff,Rd} = (0.5 \cdot A_{nt} \cdot f_u) / \gamma_{M2} + (A_{nv} \cdot f_y / 3^{1/2}) / \gamma_{M0} = 300.01 \text{ kN}$$

shear resistance total: $V_{Rd,5} = 2 \cdot V_{eff,Rd} = 600.0 \text{ kN}$

angle leg 1 in bending and shear:

$b_F = 260.0 \text{ mm} < 2.73 \cdot z = 409.5 \text{ mm}$:

shear resistance total: $V_{Rd,6} = 2 \cdot V_{Rd} = 423.6 \text{ kN}$

angle leg 1 with buckling:

$z_F = 150.0 \text{ mm} > t_F/0.15 = 80.0 \text{ mm}$:

buckling of anglechenkel 1s ist gesondert zu untersuchen !!

beam web (sb) with bearing resistance:

design bearing resistance total: $V_{Rd,8} = 106.0 \text{ kN}$

beam web (sb) with shear (gross section):

shear resistance $V_{Rd} = (A_v \cdot f_y) / (3^{1/2} \cdot \gamma_{M0}) = 579.27 \text{ kN}$

shear resistance total: $V_{Rd,9} = 579.3 \text{ kN}$

beam web (sb) with shear (net section):

shear resistance $V_{Rd} = (A_{v,net} \cdot f_u) / (3^{1/2} \cdot \gamma_{M2}) = 598.37 \text{ kN}$

shear resistance total: $V_{Rd,10} = 598.4 \text{ kN}$

beam web (sb) in tension and shear (shear block):

shear resistance $V_{eff,Rd} = (0.5 \cdot A_{nt} \cdot f_u) / \gamma_{M2} + (A_{nv} \cdot f_y / 3^{1/2}) / \gamma_{M0} = 296.69 \text{ kN}$

shear resistance total: $V_{Rd,11} = 296.7 \text{ kN}$

shear resistance: min $V_{Rd,a1} = V_{Rd,8} = 106.0 \text{ kN}$

design resistance: min $V_{Rd} = 106.0 \text{ kN}$

required plate thickness of main girder web:

beam web (mg) with bearing resistance:

design bearing resistance: $V_{Rd} = 195.1 \text{ kN}$

erf $t_u = \min V_{Rd} \cdot t / V_{Rd} = 1.63 \text{ mm}$

verification of the connection

$V_{Ed} = 89.7 \text{ kN}$: $V_{Ed} / \min V_{Rd} = 0.847 < 1$ **ok.**

verification result

maximum utilization: $\max U = 0.847 < 1$ **ok.**

Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe Dezember 2010

DIN EN 1993-1-8, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-8: Bemessung von Anschlüssen;

Deutsche Fassung EN 1993-1-8:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-8/NA, Nationaler Anhang zur DIN EN 1993-1-8, Ausgabe Dezember 2010

ECCS Document No. 126: European Recommendations for the Design of Simple Joints in Steel Structures.

ECCS TC10 - Structural Connections, 2009. J.P. Jaspart, J.F. Demonceau, S. Renkin, M.L. Guillaume

Klaus Weynand, Ralf Oerder: Typisierte Anschlüsse im Stahlhochbau nach DIN EN 1993-1-8,

IS - Gelenkige Stirnplattenanschlüsse, IW - Gelenkige Winkelanschlüsse

IG - Gelenkige Winkelanschlüsse mit großem Spalt, IK - Ausklinkungen,

Stahlbau Verlags- und Service GmbH, Ausgabe 2013