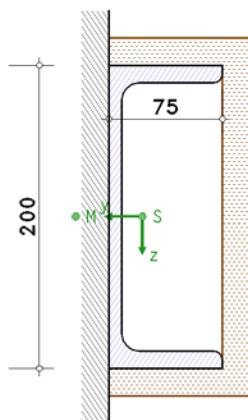


POS. 181: U-SECTION

fire design EC 3-1-2 (12.10), NA: Deutschland

1. input report



steel

steel grade S235

material safety factor

resistance of cross-sections $\gamma_{M0} = 1.00$

resistance of components in the event of fire $\gamma_{M,fi} = 1.00$

geometry

section U200

cross-section temperature

thermal action due to the standard curve, fire resistance time $t = 90 \text{ min}$

shadow effect of the section by wall/ceiling left

thermal insulation protection by plate cladding s. EC 3-1-2, appendix AA:

thermal conductivity $\lambda_p = 0.20 \text{ W/(m}\cdot\text{K)}$, specific heat capacity $c_p = 1700 \text{ J/(kg}\cdot\text{K)}$, maximum density $\rho_p = 945 \text{ kg/m}^3$

thickness of insulating material $d_p = 18.0 \text{ mm}$

resistance

plastic verification incl. c/t-verification

fire design at load level

adjustment factors for uneven temperature distribution

across the cross section $\kappa_1 = 0.85$, along the beam $\kappa_2 = 1.00$

internal forces and moments (event of fire)

σ -generating forces (N, M) work at centroid, τ -generating forces (V, T_t) work at shear center

Lk 1: $M_{y,fi} = 7.00 \text{ kNm}$, $M_{z,fi} = 5.00 \text{ kNm}$

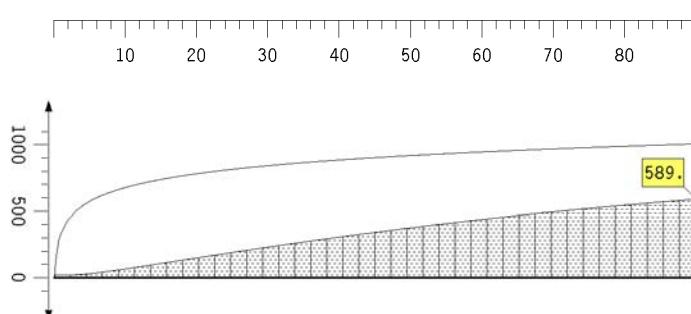
notes

stability is not investigated.

2. cross-section temperature

section factor of the protected component $A_p/V = 350.0 / 3270.8 \cdot 10^3 = 107.0 \text{ 1/m}$

temperature development:

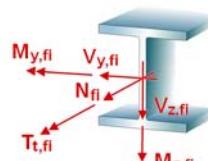


temperature in °C

fire time in min

max $T_a = 589.2^\circ\text{C}$

max $t = 90 \text{ min}$



cross-section temperature acc. to $t = 90 \text{ min}$: $T_a = 589.2^\circ\text{C}$

material parameters: $f_y,fi = 118.3 \text{ N/mm}^2$, $E_{fi} = 71648.0 \text{ N/mm}^2$, $\alpha_{T,fi} = 1.44 \cdot 10^{-5} \text{ 1/K}$

3. Lk 1

3.1. fire design

3.1.1. plastic verification

3.1.1.1. verification at load level

plastic verification for $M_y = 5.95 \text{ kNm}$, $M_z = 4.25 \text{ kNm}$

max. load factor of normal stresses (plastic): $f_{\sigma,pl} = 1.109 \Rightarrow U_{\sigma,pl} = 0.902$

verification: $U_{pl} = 0.902 < 1 \text{ ok}$

c/t-verification: utilization $U_{c/t} = 0.550 < 1 \text{ ok}$

4. final result

maximum utilization:	stress	$\max U_{\sigma} = 0.902 < 1 \text{ ok}$
	c/t-ratio	$\max U_{c/t} = 0.550 < 1 \text{ ok}$
	resistance	$\max U = 0.902 < 1 \text{ ok}$

verification succeeded

5. Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1991-1-2, Eurocode 1: Einwirkungen auf Tragwerke - Teil 1-2: Allgemeine Einwirkungen -

Brandeinwirkungen auf Tragwerke; Deutsche Fassung EN 1991-1-2, Ausgabe Dezember 2010

DIN EN 1991-1-2/NA, Nationaler Anhang zur DIN EN 1991-1-2, Ausgabe September 2015

DIN EN 1993-1-2, Eurocode 3: Bemessung und Konstruktion von Stahlbauten - Teil 1-2: Allgemeine Regeln -

Tragwerksbemessung für den Brandfall; Deutsche Fassung EN 1993-1-2, Ausgabe Dezember 2010

DIN EN 1993-1-2/NA, Nationaler Anhang zur DIN EN 1993-1-2, Ausgabe Dezember 2010