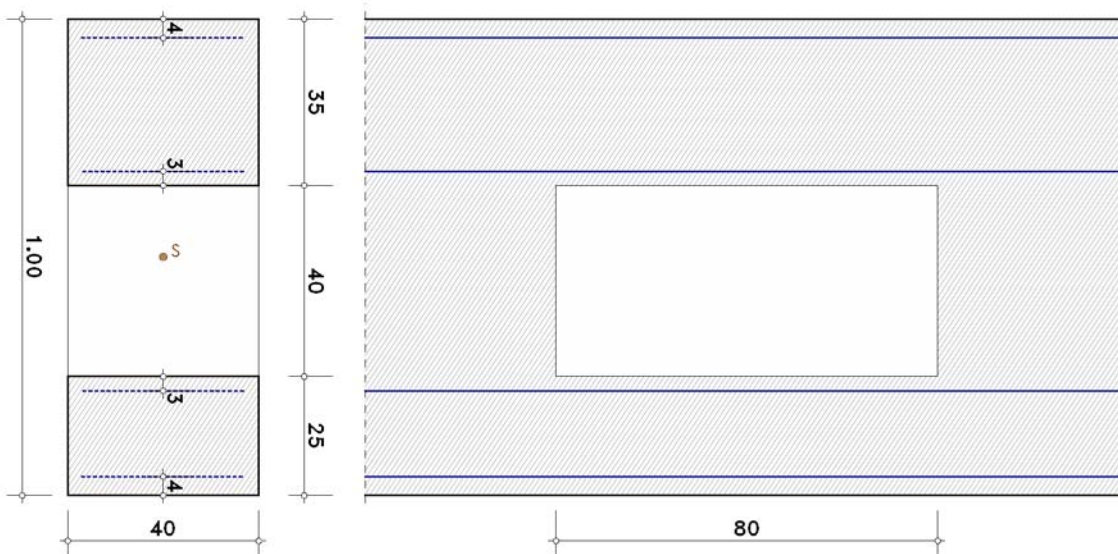


1. input protocol



cross section

rectangle: $h = 100.0$ cm, $b = 40.0$ cm

recess: $e_o = 35.0$ cm, $e_u = 25.0$ cm, $l_A = 80.0$ cm

axis distances (calculation): $d_{o,o} = 4.0$ cm, $d_{u,o} = 3.0$ cm, $d_{o,u} = 3.0$ cm, $d_{u,u} = 4.0$ cm

material properties

concrete acc. to EC 2, 3.1.7(1): C30/37, $\epsilon_{c2} = -2.00\%$, $\epsilon_{cu2} = -3.50\%$, $f_{cd} = 17.00$ N/mm²

reinforcement acc. to EC 2, 3.2.7(2a): B500A, $\epsilon_{sd} = 25.0\%$, $f_{yd} = 434.78$ N/mm², $f_{td} = 456.52$ N/mm², $E_s = 200000.0$ N/mm²

parameters

base reinforcement: top chord above $A_{so,o} = 0.00$ cm², bottom chord bottom $A_{su,o} = 6.00$ cm²

design method acc. to Heft 399, DAfStb

moment zero crossing in the centre of recess

shear force distribution determined from the effective belt stiffnesses

shear design: compression strut angle minimum

1.1. design calculation values

lc 1: $M_{y,Ed} = 168.00$ kNm, $V_{z,Ed} = -330.00$ kN

2. note

general reinforcement rules are not taken into account.

3. recess

3.1. lc 1

recess close to bearing (IM/VI < 1 m): method may not be suitable !

design calculation values in centre cut: $N_{Ed} = 0.00$ kN, $M_{Ed} = 168.00$ kNm, $V_{Ed} = -330.00$ kN

shear force distribution: 80.8% of shear force acts in the compression chord (= top chord)

above the recess

design calculation values in top chord: $N_{Ed,o} = -205.9$ kN, $V_{Ed,o} = -266.8$ kN, $M_{Ed,o} = \pm 106.7$ kNm

longitudinal reinforcement in top chord: $A_{so,o} = 6.52$ cm², $A_{su,o} = 6.24$ cm²

shear design:

design resistance without shear reinforcement $V_{Rdc} = 79.44$ kN, max. design resistance of compression strut $V_{Rd,mx} = 587.39$ kN

$V_{Rdc} < |V_{Ed,o}| < V_{Rd,mx} \Rightarrow$ shear reinforcement in top chord: $a_{sb,o} = 12.38$ cm²/m

below the recess

design calculation values in bottom chord: $N_{Ed,u} = 205.9$ kN, $V_{Ed,u} = -63.2$ kN, $M_{Ed,u} = \pm 25.3$ kNm

longitudinal reinforcement in bottom chord: $A_{so,u} = 5.09$ cm², $A_{su,u} = 5.34$ cm²

shear design:

design resistance without shear reinforcement $V_{Rdc} = 22.70$ kN, max. design resistance of compression strut $V_{Rd,mx} = 275.40$ kN

$V_{Rdc} < |V_{Ed,u}| < V_{Rd,mx} \Rightarrow$ shear reinforcement in bottom chord $a_{sb,u} = 3.71$ cm²/m

suspended reinforcement: $T_{v,l} = 492.3$ kN $\Rightarrow A_{s,l} = 11.32$ cm², $T_{v,r} = 135.9$ kN $\Rightarrow A_{s,r} = 3.13$ cm², distribution width 30.0 cm

total: $A_{so,o} = 6.52$ cm², $A_{su,o} = 6.24$ cm², $a_{sb,o} = 12.38$ cm²/m, $A_{so,u} = 5.09$ cm², $A_{su,u} = 5.34$ cm²

$a_{sb,u} = 3.71$ cm²/m, $A_{s,l} = 11.32$ cm², $A_{s,r} = 3.13$ cm², $\rho = 0.58\%$

4. final result

maximum reinforcement: $A_{so,o} = 6.52 \text{ cm}^2$, $A_{su,o} = 6.24 \text{ cm}^2$, $a_{sb,o} = 12.38 \text{ cm}^2/\text{m}$, $A_{so,u} = 5.09 \text{ cm}^2$
 $A_{su,u} = 5.34 \text{ cm}^2$, $a_{sb,u} = 3.71 \text{ cm}^2/\text{m}$, $A_{s,l} = 11.32 \text{ cm}^2$, $A_{s,r} = 3.13 \text{ cm}^2$, $\rho = 0.58\%$
incl. base reinforcement: $A_{so,o} = 6.52 \text{ cm}^2$, $A_{su,o} = 6.00 \text{ cm}^2$

design resistance ensured

5. regulations

EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;
Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010
EN 1990/NA, Nationaler Anhang zur EN 1990, Ausgabe Dezember 2010

EN 1992-1-1, Eurocode 2: Bemessung und Konstruktion von Stahlbeton- und Spannbetonbauteilen -
Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;
Deutsche Fassung EN 1992-1-1:2004 + AC:2010, Ausgabe Januar 2011
EN 1992-1-1/NA, Nationaler Anhang zur EN 1992-1-1, Ausgabe April 2013

Rolf Eligehausen, Roland Gerster: Das Bewehren von Stahlbetonbauteilen,
Deutscher Ausschuss für Stahlbeton, Heft 399, Beuth Verlag GmbH, 1993