

1. Input parameters

1.1. girder opening rectangular with glued on reinforcements acc. to DIN EN 1995-1-1/NA:2013-08, NCI NA.6.8.4

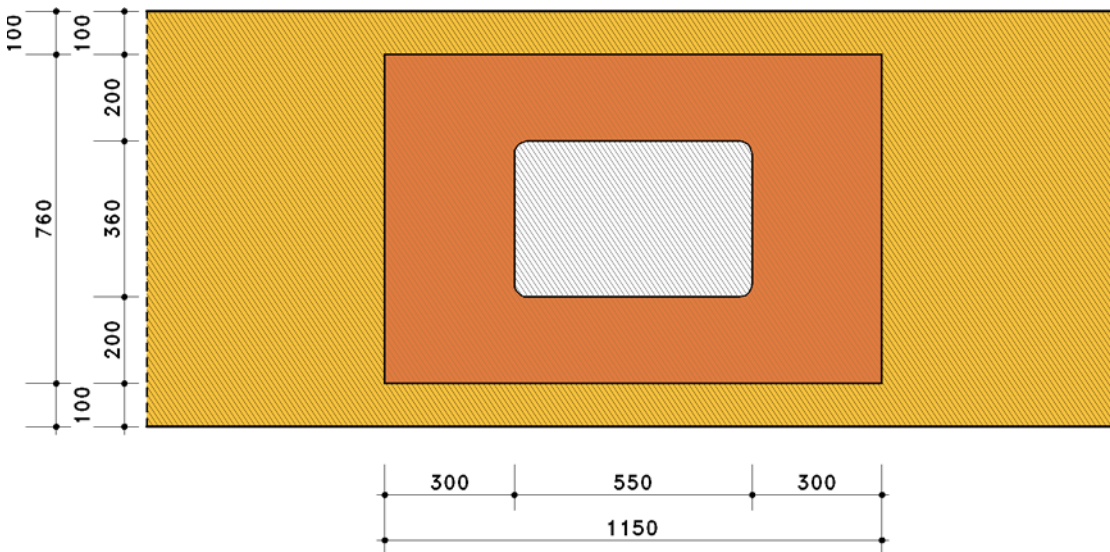
1.2. beam

beam of glue laminated timber EC, GL24h 200/960 mm, $\rho_k = 385 \text{ kg/m}^3$, NKL 1
 $h_{ro} = 300 \text{ mm}$, $h_{ru} = 300 \text{ mm}$, $a = 550 \text{ mm}$ (expressions acc. to NA:2013-08, NCI NA.6.7 figure NA.7)
 $f_{m,k} = 24.00 \text{ N/mm}^2$, $f_{t,k} = 19.20 \text{ N/mm}^2$, $f_{c,k} = 24.00 \text{ N/mm}^2$, $f_{v,k} = 3.50 \text{ N/mm}^2$, $f_{t90,k} = 0.50 \text{ N/mm}^2$
 filleting of opening edges with $r \geq 15 \text{ mm}$ $r \geq \#\#\# \text{ mm}$
 $f_{m,k}$ increased with $k_h = 1.000$

1.3. reinforcement by glued lugs

plywood F40/30 $a_r = 300 \text{ mm}$, $h_l = 200 \text{ mm}$, $t_r = 12 \text{ mm}$, $f_{t,k} = 29.00 \text{ N/mm}^2$ parallel to the grain direction of the face

elevation scale 1:175, unit of length [mm]



1.4. internal forces and moments

Nr.	name	left edge			right edge			KLED	Kmod	γ
		Nd kN	Vd kN	Md kNm	Nd kN	Vd kN	Md kNm			
1	g+t+s	0.00	0.00	924.80	0.00	88.00	900.60	med.-term	0.800	1.30

2. results

2.1. tension stress perpendicular to grain in opening area

$f_{k2,k} = 0.75 \text{ N/mm}^2$ (table NA.12)

Nr	$f_{t90,d}$ N/mm ²	$f_{k2,d}$ N/mm ²	$f_{t,d}$ N/mm ²	left edge							
				$F_{tV,d}$ kN	$F_{tM,d}$ kN	$F_{t90,d}$ kN	$\tau_{ref,d}$ N/mm ²	$\sigma_{t,d}$ N/mm ²	$u_{ref,d}$ -	$u_{\sigma,d}$ -	u_l -
1	0.308	0.462	17.85	0.00	24.66	24.66	0.206	3.43	0.445	0.384	0.445

Nr	$f_{t90,d}$ N/mm ²	$f_{k2,d}$ N/mm ²	$f_{t,d}$ N/mm ²	right edge								
				$F_{tV,d}$ kN	$F_{tM,d}$ kN	$F_{t90,d}$ kN	$\tau_{ref,d}$ N/mm ²	$\sigma_{t,d}$ N/mm ²	$u_{ref,d}$ -	$u_{\sigma,d}$ -	u_r kN	u -
1	0.308	0.462	17.85	23.59	24.02	47.61	0.397	6.61	0.860	0.741	0.860	0.860

$u_{max} = 0.860 \leq 1 \Rightarrow \text{ok.}$

2.2. bending at the opening area cross-section

$I_{nz} = 1396800 \text{ cm}^4$, $z_s = 480 \text{ mm}$, $W_{no} = 29100 \text{ cm}^3$, $W_{nu} = 29100 \text{ cm}^3$, $W_o = 3000 \text{ cm}^3$, $W_u = 3000 \text{ cm}^3$

Nr	$f_{m,d}$ N/mm ²	$f_{t,d}$ N/mm ²	$f_{c,d}$ N/mm ²	$\sigma_{N,d}$ N/mm ²	$\sigma_{M,o,d}$ N/mm ²	$\sigma_{M,u,d}$ N/mm ²	$\Delta\sigma_{M,o,d}$ N/mm ²	$\Delta\sigma_{M,u,d}$ N/mm ²	$\sigma_{u,d}$ N/mm ²	$\sigma_{o,d}$ N/mm ²	$u_{o,d}$ -	$u_{u,d}$ -	u -

$u_{max} = 2.260 > 1 \Rightarrow \text{not ok. !!}$

2.3. shear at the reduced cross section

beam width = 200 mm, beam height = 600 mm, $k_{cr} = 0.714 \Rightarrow A_{ef} = 85714 \text{ mm}^2$, $\kappa_{max} = 2.379$

Nr	$f_{v,d}$ N/mm ²	left edge			right edge			u -
		V_d kN	$\tau_{m,d}$ N/mm ²	u -	V_d kN	$\tau_{m,d}$ N/mm ²	u -	
1	2.15	0.00	0.000	0.000	88.00	3.663	1.701	1.701

$u_{max} = 1.701 > 1 \Rightarrow$ not ok. !!

3. Summary

total utilization all verifications $u_{max,Ges} = 2.260 > 1 \Rightarrow$ not ok. !!