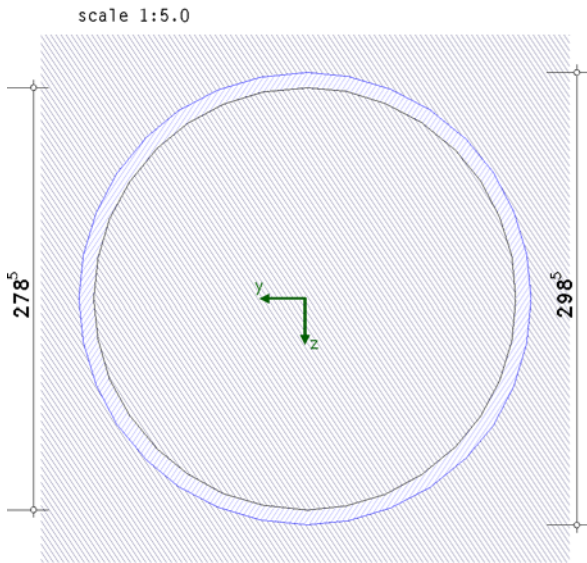


Welded connection

DIN 18800 (11.08)



material

steel grade S 235

material safety factor $\gamma_M = 1.10$

geometry

section R298.5X10.0

plate: thickness $t_p = 35.0$ mm

surrounding fillet weld: $a_w = 5.0$ mm, 75% decrease of the axial force by pressure contact

design resistance

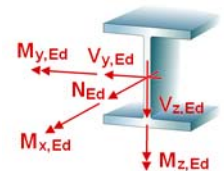
elastic cross-sectional check

internal forces and moments and utilizations

$N_{Ed}, V_{z,Ed}, M_{z,Ed}, V_{y,Ed}, M_{x,Ed}$: internal forces and moments by sign definition of statics

U_σ : stress utilization of cross section, U_w : stress utilization of welds

Lk	N_{Ed} kN	$V_{z,Ed}$ kN	$M_{z,Ed}$ kNm	$V_{y,Ed}$ kN	$M_{x,Ed}$ kNm	U_σ	U_w	
--								
1	-82.12	-5.56	51.11	37.78	22.23	0.432	0.801*	Lf 1
2	-38.25	-0.08	36.27	-2.93	0.31	0.282	0.539	Lf 2
3	-65.61	-2.54	12.06	20.82	10.14	0.136	0.243	Lf 7



Final result

maximum utilization [Lk 1]: design resistance max $U = 0.801 < 1$ **ok.**

verification succeeded

Regulations

DIN 18800-1: Stahlbauten - Teil 1: Bemessung und Konstruktion, Ausgabe November 2008

steel section

dimensions and cross-sectional properties (thick-walled)

$$\begin{aligned} d &= 298.5 \text{ mm} & t &= 10.0 \text{ mm} \\ A &= 90.6 \text{ cm}^2 & I_y &= 9441.0 \text{ cm}^4 & I_z &= 9441.0 \text{ cm}^4 & I_T &= 18882.0 \text{ cm}^4 \\ W_y &= 632.6 \text{ cm}^3 & W_z &= 632.6 \text{ cm}^3 \end{aligned}$$

stresses

$$\sigma_{\max} = 71.7 \text{ N/mm}^2 \quad \sigma_{\min} = -89.9 \text{ N/mm}^2 \quad \tau_{\max} = 8.3 \text{ N/mm}^2 \quad \sigma_v = 94.3 \text{ N/mm}^2$$

utilization ($\sigma_{R,d} = 218.2 \text{ N/mm}^2$ $\tau_{R,d} = 126.0 \text{ N/mm}^2$)

$$\sigma/\sigma_{R,d} = 0.41 < 1 \quad \tau/\tau_{R,d} = 0.07 < 1 \quad \sigma_v/\sigma_{R,d} = 0.43 < 1$$

welds

cross-sectional properties (not full-sized)

$$A_w = 46.9 \text{ cm}^2 \quad I_{yw} = 5222.3 \text{ cm}^4 \quad I_{zw} = 5222.3 \text{ cm}^4 \quad I_{Tw} = 10444.6 \text{ cm}^4 \quad W_{Tw} = 699.8 \text{ cm}^3$$

weld-stresses

$$\begin{aligned} \sigma_{w,\max} &= 128.69 \text{ N/mm}^2 & \sigma_{w,\min} &= -163.45 \text{ N/mm}^2 & \tau_w &= 16.11 \text{ N/mm}^2 & \tau_{Tw} &= 31.77 \text{ N/mm}^2 \\ \sigma_{w,v} &= 166.07 \text{ N/mm}^2 \end{aligned}$$

utilization ($\alpha_w = 0.95$ $\sigma_{w,R,d} = 207.3 \text{ N/mm}^2$)

$$\sigma/\sigma_{w,R,d} = 0.79 < 1 \quad \tau/\sigma_{w,R,d} = 0.08 < 1 \quad \sigma_{w,v}/\sigma_{w,R,d} = 0.80 < 1$$

all required verifications are verified!