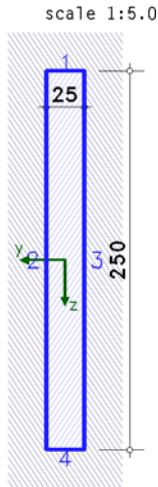


Welded connection

EC 3-1-8 (12.10), NA: Deutschland



material

steel grade S 235

geometry

section parameters (flat steel):

length $h = 250.0$ mm, thickness $t = 25.0$ mm

plate: thickness $t_p = 35.0$ mm

welds as fillet weld:

$a_{w1} = 6.0$ mm, $l_{w1} = 25.0$ mm $a_{w2} = 6.0$ mm, $l_{w2} = 250.0$ mm $a_{w3} = 6.0$ mm, $l_{w3} = 250.0$ mm

$a_{w4} = 6.0$ mm, $l_{w4} = 25.0$ mm

design resistance

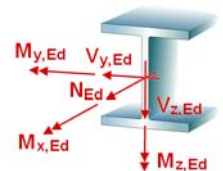
elastic cross-sectional check

weld verification with the simplified method

resolution of shear force is made by the stiffness of the single weld.

internal forces and moments (sign definition of statics)

Lk 1: $N_{Ed} = 1.90$ kN $V_{z,Ed} = -2.87$ kN $M_{z,Ed} = 4.26$ kNm



Lk 1:

cross-sectional check

design values: $N_{Ed} = 1.90$ kN, $V_{z,Ed} = -2.87$ kN, $M_{z,Ed} = 4.26$ kNm

elastic stresses: $\max \sigma_x = 163.9$ N/mm², $\min \sigma_x = -163.3$ N/mm², $\max \tau = 0.7$ N/mm², $\max \sigma_v = 163.9$ N/mm²

valid stresses: $\sigma_{Rd} = 235.0$ N/mm², $\tau_{Rd} = 135.7$ N/mm²

utilizations: design resistance $U_\sigma = 0.697 < 1$ **ok**.

verification of welds

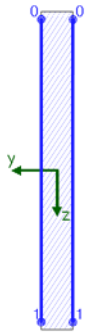
calculation section:

weld 1: effective weld length $l_{eff} = 13.0$ mm < 30 mm \Rightarrow has no effect !!

weld 1: effective weld length $l_{eff} = 13.0$ mm $< 6 \cdot a = 36.0$ mm \Rightarrow has no effect !!

weld 4: effective weld length $l_{eff} = 13.0$ mm < 30 mm \Rightarrow has no effect !!

weld 4: effective weld length $l_{eff} = 13.0$ mm $< 6 \cdot a = 36.0$ mm \Rightarrow has no effect !!



weld 2: $a_w = 6.0 \text{ mm}$ $l_w = 238.0 \text{ mm}$
weld 3: $a_w = 6.0 \text{ mm}$ $l_w = 238.0 \text{ mm}$

design values:

$N_{Ed} = 1.90 \text{ kN}$, $V_{z,Ed} = -2.87 \text{ kN}$, $M_{z,Ed} = 4.26 \text{ kNm}$

cross-sectional properties referring to centroid of the line cross section:

$\Sigma A_w = 28.56 \text{ cm}^2$, $\Sigma l_w = 47.6 \text{ cm}$

$I_{w,y} = 1348.13 \text{ cm}^4$, $I_{w,z} = 45.48 \text{ cm}^4$, $\Delta y_w = 0.0 \text{ mm}$, $\Delta z_w = 0.0 \text{ mm}$

member forces distributed to the individual welds:

weld 2: $N_w = -166.24 \text{ kN}$ $M_{z,w} = 0.04 \text{ kNm}$ $V_{z,w} = -1.44 \text{ kN}$

weld 3: $N_w = 168.14 \text{ kN}$ $M_{z,w} = 0.04 \text{ kNm}$ $V_{z,w} = -1.44 \text{ kN}$

verifications in the edge points of the individual welds:

weld 2, pt. 0: $\sigma_{w,x} = -116.41 \text{ N/mm}^2$ $\tau_{w,z} = 1.00 \text{ N/mm}^2$ $\Rightarrow U_w = 0.560 < 1$ **ok.**

pt. 1: $\sigma_{w,x} = -116.41 \text{ N/mm}^2$ $\tau_{w,z} = 1.00 \text{ N/mm}^2$ $\Rightarrow U_w = 0.560 < 1$ **ok.**

weld 3, pt. 0: $\sigma_{w,x} = 117.75 \text{ N/mm}^2$ $\tau_{w,z} = 1.00 \text{ N/mm}^2$ $\Rightarrow U_w = 0.567 < 1$ **ok.**

pt. 1: $\sigma_{w,x} = 117.75 \text{ N/mm}^2$ $\tau_{w,z} = 1.00 \text{ N/mm}^2$ $\Rightarrow U_w = 0.567 < 1$ **ok.**

Result:

weld 3, pt. 0: $\sigma_{w,x} = 117.75 \text{ N/mm}^2$ $\tau_{w,z} = 1.00 \text{ N/mm}^2$
 $F_{w,Ed} = 7.06 \text{ kN/cm} < F_{w,Rd} = 12.47 \text{ kN/cm} \Rightarrow U_w = 0.567 < 1$ **ok.**

Final result

maximum utilization: design resistance $\max U = 0.697 < 1$ **ok.**

verification succeeded