

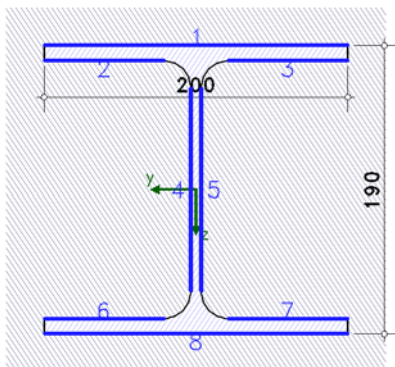
POS. 1: I-SECTION, EC3, TABLE

4H-EC3SA version: 10/2014-1m

Welded connection

EC 3-1-8 (12.10), NA: Deutschland

scale 1:5.0



material

steel grade S 235

partial safety factors for material

resistance of cross sections $\gamma_{M0} = 1.00$

resistance of bolts, welds, plates in bearing $\gamma_{M2} = 1.25$

geometry

section HE200A

plate: thickness $t_p = 35.0$ mm

welds as fillet weld:

$a_{w1} = 6.0$ mm, $l_{w1} = 200.0$ mm

$a_{w1} = 3.0$ mm, $l_{w1} = 200.0$ mm

$a_{w2} = 6.0$ mm, $l_{w2} = 78.8$ mm

$a_{w3} = 6.0$ mm, $l_{w3} = 78.8$ mm

$a_{w4} = 6.0$ mm, $l_{w4} = 134.0$ mm

$a_{w5} = 6.0$ mm, $l_{w5} = 134.0$ mm

$a_{w6} = 6.0$ mm, $l_{w6} = 78.8$ mm

$a_{w7} = 6.0$ mm, $l_{w7} = 78.8$ mm

$a_{w8} = 6.0$ mm, $l_{w8} = 200.0$ mm

$a_{w8} = 3.0$ mm, $l_{w8} = 200.0$ mm

length of welds is not checked.

design resistance

elastic cross-sectional check

weld verification with the simplified method

resolution of shear force is made by the stiffness of the single weld.

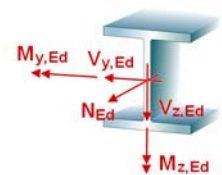
internal forces and moments and utilizations

$N_{Ed}, V_{z,Ed}, M_{z,Ed}, V_{y,Ed}$: internal forces and moments by sign definition of statics

U_{σ} : stress utilization of cross section, U_w : stress utilization of welds

$U_{c/t}$: c/t-utilization of cross section

Lk	N_{Ed} kN	$V_{z,Ed}$ kN	$M_{z,Ed}$ kNm	$V_{y,Ed}$ kN	U_{σ}	$U_{c/t}$	U_w
1	8.44	-2.30	-2.65	6.54	0.091	0.136	0.100
2	14.15	-6.21	21.68	5.42	0.700	0.408	0.759*
3	-11.73	2.06	-16.15	7.96	0.522	0.360	0.566



Final result

maximum utilization [Lk 2]:

design resistance max $U = 0.759 < 1$ ok.

c/t-ratio max $U = 0.408 < 1$ ok.

verification succeeded

Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;
 Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010
 DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -
 Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;
 Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010
 DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe Dezember 2010

DIN EN 1993-1-8, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -
 Teil 1-8: Bemessung von Anschlüssen;
 Deutsche Fassung EN 1993-1-8:2005 + AC:2009, Ausgabe Dezember 2010
 DIN EN 1993-1-8/NA, Nationaler Anhang zur DIN EN 1993-1-8, Ausgabe Dezember 2010

Detailed edition

Lk 2:

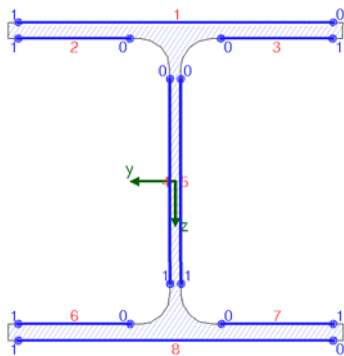
cross-sectional check

design values: $N_{Ed} = 14.15 \text{ kN}$, $V_{z,Ed} = -6.21 \text{ kN}$, $M_{z,Ed} = 21.68 \text{ kNm}$, $V_{y,Ed} = 5.42 \text{ kN}$
 elastic stresses: $\max \sigma_x = 164.5 \text{ N/mm}^2$, $\min \sigma_x = -159.2 \text{ N/mm}^2$, $\max \tau = 5.5 \text{ N/mm}^2$, $\max \sigma_v = 164.5 \text{ N/mm}^2$
 valid stresses: $\sigma_{Rd} = 235.0 \text{ N/mm}^2$, $\tau_{Rd} = 135.7 \text{ N/mm}^2$
 utilizations: design resistance $U_\sigma = 0.700 < 1$ **ok.**, c/t -ratio $U_{c/t} = 0.408 < 1$ **ok.**

verification of welds

calculation section:

weld 4: weld thickness $a = 6.0 \text{ mm} > a_{\max} = t_{\min} = 4.6 \text{ mm} \quad !!$
 weld 5: weld thickness $a = 6.0 \text{ mm} > a_{\max} = t_{\min} = 4.6 \text{ mm} \quad !!$



weld 1:	$a_w = 6.0 \text{ mm}$	$l_w = 188.0 \text{ mm}$
weld 2:	$a_w = 6.0 \text{ mm}$	$l_w = 66.8 \text{ mm}$
weld 3:	$a_w = 6.0 \text{ mm}$	$l_w = 66.8 \text{ mm}$
weld 4:	$a_w = 6.0 \text{ mm}$	$l_w = 122.0 \text{ mm}$
weld 5:	$a_w = 6.0 \text{ mm}$	$l_w = 122.0 \text{ mm}$
weld 6:	$a_w = 6.0 \text{ mm}$	$l_w = 66.8 \text{ mm}$
weld 7:	$a_w = 6.0 \text{ mm}$	$l_w = 66.8 \text{ mm}$
weld 8:	$a_w = 6.0 \text{ mm}$	$l_w = 188.0 \text{ mm}$

design values:

$N_{Ed} = 14.15 \text{ kN}$, $V_{z,Ed} = -6.21 \text{ kN}$, $M_{z,Ed} = 21.68 \text{ kNm}$, $V_{y,Ed} = 5.42 \text{ kN}$

cross-sectional properties referring to centroid of the line cross section:

$\Sigma A_w = 53.22 \text{ cm}^2$, $\Sigma l_w = 88.7 \text{ cm}$

$I_{w,y} = 3376.23 \text{ cm}^4$, $I_{w,z} = 1314.73 \text{ cm}^4$, $\Delta y_w = 0.0 \text{ mm}$, $\Delta z_w = 0.0 \text{ mm}$

member forces distributed to the individual welds:

weld 1:	$N_w = 3.00 \text{ kN}$	$M_{z,w} = 5.48 \text{ kNm}$	$V_{y,w} = 2.49 \text{ kN}$	$V_{z,w} = -0.01 \text{ kN}$
weld 2:	$N_w = -38.98 \text{ kN}$	$M_{z,w} = 0.25 \text{ kNm}$	$V_{y,w} = 0.11 \text{ kN}$	$V_{z,w} = -0.00 \text{ kN}$
weld 3:	$N_w = 41.11 \text{ kN}$	$M_{z,w} = 0.25 \text{ kNm}$	$V_{y,w} = 0.11 \text{ kN}$	$V_{z,w} = -0.00 \text{ kN}$
weld 4:	$N_w = -1.98 \text{ kN}$	$M_{z,w} = 0.00 \text{ kNm}$	$V_{y,w} = 0.00 \text{ kN}$	$V_{z,w} = -3.09 \text{ kN}$
weld 5:	$N_w = 5.87 \text{ kN}$	$M_{z,w} = 0.00 \text{ kNm}$	$V_{y,w} = 0.00 \text{ kN}$	$V_{z,w} = -3.09 \text{ kN}$
weld 6:	$N_w = -38.98 \text{ kN}$	$M_{z,w} = 0.25 \text{ kNm}$	$V_{y,w} = 0.11 \text{ kN}$	$V_{z,w} = -0.00 \text{ kN}$
weld 7:	$N_w = 41.11 \text{ kN}$	$M_{z,w} = 0.25 \text{ kNm}$	$V_{y,w} = 0.11 \text{ kN}$	$V_{z,w} = -0.00 \text{ kN}$
weld 8:	$N_w = 3.00 \text{ kN}$	$M_{z,w} = 5.48 \text{ kNm}$	$V_{y,w} = 2.49 \text{ kN}$	$V_{z,w} = -0.01 \text{ kN}$

verifications in the edge points of the individual welds:

weld 1,	pt. 0:	$\sigma_{w,x} = 157.69 \text{ N/mm}^2$	$\tau_{w,y} = 2.20 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.759 < 1$ ok.
	pt. 1:	$\sigma_{w,x} = -152.38 \text{ N/mm}^2$	$\tau_{w,y} = 2.20 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.733 < 1$ ok.
weld 2,	pt. 0:	$\sigma_{w,x} = -42.28 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.203 < 1$ ok.
	pt. 1:	$\sigma_{w,x} = -152.38 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.733 < 1$ ok.
weld 3,	pt. 0:	$\sigma_{w,x} = 47.60 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.229 < 1$ ok.
	pt. 1:	$\sigma_{w,x} = 157.69 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.759 < 1$ ok.

weld 4,	pt. 0:	$\sigma_{w,x} = -2.70 \text{ N/mm}^2$	$\tau_{w,y} = 0.00 \text{ N/mm}^2$	$\tau_{w,z} = 4.21 \text{ N/mm}^2$	$\Rightarrow U_w = 0.024 < 1$	ok.
	pt. 1:	$\sigma_{w,x} = -2.70 \text{ N/mm}^2$	$\tau_{w,y} = 0.00 \text{ N/mm}^2$	$\tau_{w,z} = 4.21 \text{ N/mm}^2$	$\Rightarrow U_w = 0.024 < 1$	ok.
weld 5,	pt. 0:	$\sigma_{w,x} = 8.02 \text{ N/mm}^2$	$\tau_{w,y} = 0.00 \text{ N/mm}^2$	$\tau_{w,z} = 4.21 \text{ N/mm}^2$	$\Rightarrow U_w = 0.044 < 1$	ok.
	pt. 1:	$\sigma_{w,x} = 8.02 \text{ N/mm}^2$	$\tau_{w,y} = 0.00 \text{ N/mm}^2$	$\tau_{w,z} = 4.21 \text{ N/mm}^2$	$\Rightarrow U_w = 0.044 < 1$	ok.
weld 6,	pt. 0:	$\sigma_{w,x} = -42.28 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.203 < 1$	ok.
	pt. 1:	$\sigma_{w,x} = -152.38 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.733 < 1$	ok.
weld 7,	pt. 0:	$\sigma_{w,x} = 47.60 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.229 < 1$	ok.
	pt. 1:	$\sigma_{w,x} = 157.69 \text{ N/mm}^2$	$\tau_{w,y} = 0.28 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.759 < 1$	ok.
weld 8,	pt. 0:	$\sigma_{w,x} = 157.69 \text{ N/mm}^2$	$\tau_{w,y} = 2.20 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.759 < 1$	ok.
	pt. 1:	$\sigma_{w,x} = -152.38 \text{ N/mm}^2$	$\tau_{w,y} = 2.20 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$	$\Rightarrow U_w = 0.733 < 1$	ok.
Result:						
weld 1,	pt. 0:	$\sigma_{w,x} = 157.69 \text{ N/mm}^2$	$\tau_{w,y} = 2.20 \text{ N/mm}^2$	$\tau_{w,z} = 0.01 \text{ N/mm}^2$		
		$F_{w,Ed} = 9.14 \text{ kN/cm} < F_{w,Rd} = 12.47 \text{ kN/cm} \Rightarrow U_w = 0.759 < 1$				ok.