

# POS. 9: TYPED IW-CONNECTION

## standard IW-connection

hinged IW-connection acc. to EC 3-1-8 (12.10), NA: Deutschland

the connection type, dimensions of beam, bolts, end-plate resp. angle and material are taken of the following literature:

'Typisierte Anschlüsse im Stahlhochbau nach DIN EN 1993-1-8, Stahlbau Verlags- und Service GmbH, Ausgabe 2013' the current number and associated parameters are recorded. verification method is 'elastic-elastic'. bolts are not preloaded.

code IW, steel grade S 235, bolt class of bolts 4.6

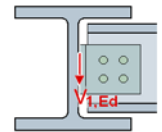
78: beam section IPE300, connection type 1, bolt size M20, 3 bolt-rows

angle: L100X10,  $h_{wi} = 220$  mm,  $w_t = 128$  mm

$e_{z,mg} = 40$  mm,  $p_{z,mg} = 70$  mm,  $e_{x,mg} = 40$  mm,  $e_{z,sb} = 40$  mm,  $p_{z,sb} = 70$  mm,  $e_{x,sb} = 40$  mm

$V_{j,Ed}$ : internal forces and moments at hinge

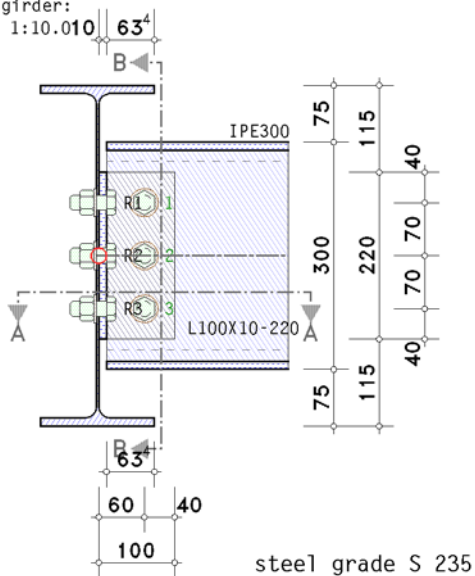
Lk	$V_{j,Ed}$ kN		Lk	$V_{j,Ed}$ kN		Lk	$V_{j,Ed}$ kN	
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1	27.22	min N	5	-6.85	min $V_{\zeta}$	9	-22.74	min $V_{\eta}$
2	89.08	max N	6	63.25	min $\sigma_l$	10	-79.40	min $V_{\zeta}$
3	26.19	min $V_{\eta}$	7	-68.00	min N	11	-4.22	max $V_{\zeta}$
4	89.70	max $V_{\eta}$	8	-23.21	max N			



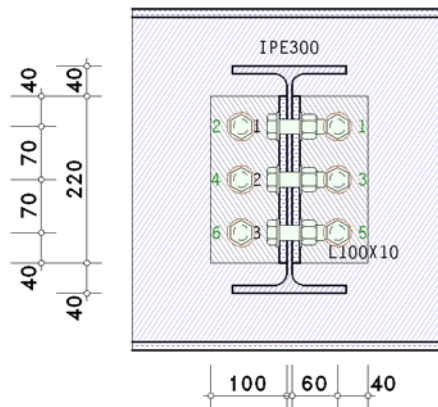
## Simple Joint of Beams

EC 3-1-8 (12.10), NA: Deutschland

main girder:  
scale 1:10.010

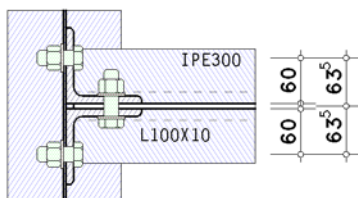


section B-B:



○ hinge

section A-A:



steel grade S 235  
bolts M20-4.6

## partial safety factors for material

resistance of cross sections  $\gamma_{M0} = 1.00$

resistance of bolts, welds, plates in bearing  $\gamma_{M2} = 1.25$

resistance with tension loads  $\gamma_{Mu} = 1.10$

## Final Result

maximum utilization [Lk 4]: design resistance max U = 0.451 < 1 **ok**.

verification succeeded

## Decisive load case combination

notes

design resistance of the main girder is not verified.

distances between bolts are not checked.

### Lk 4: max $V_{\eta}$

## design values

transformation of member forces to the reference point (intersection point of beam axis')

$$M_{1,Ed} = V_{j1,Ed} \cdot e_1 = -0.15 \text{ kNm}, \quad e_1 = -1.6 \text{ mm}$$

$$V_{1,Ed} = V_{j1,Ed} = 89.70 \text{ kN}$$

## design resistance of the connection

### angle leg at main girder:

shear force resistance

bolts in shear:

$$\text{design shear resistance per shear plane: } F_{v,Rd} = \alpha_v \cdot f_{ub} \cdot A / \gamma_{M2} = 60.32 \text{ kN}, \quad \alpha_v = 0.60$$

$$\text{design shear resistance total: } V_{Rd,1} = 260.1 \text{ kN}$$

angle leg 2 with bearing resistance:

$$\text{design bearing resistance total: } V_{Rd,2} = 423.4 \text{ kN}$$

angle leg 2 with shear (gross section):

$$\text{shear resistance } V_{Rd} = (A_v \cdot f_y) / (3^{1/2} \cdot \gamma_{M0}) = 298.49 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,3} = 2 \cdot V_{Rd} / 1.27 = 470.1 \text{ kN}$$

angle leg 2 with shear (net section):

$$\text{shear resistance } V_{Rd} = (A_{v,net} \cdot f_u) / (3^{1/2} \cdot \gamma_{M2}) = 256.07 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,4} = 2 \cdot V_{Rd} = 512.1 \text{ kN}$$

$$\text{shear resistance: } \min V_{Rd,a2} = V_{Rd,1} = 260.1 \text{ kN}$$

### angle leg at supported beam:

shear force resistance

bolts in shear:

$$\text{design shear resistance per shear plane: } F_{v,Rd} = \alpha_v \cdot f_{ub} \cdot A / \gamma_{M2} = 60.32 \text{ kN}, \quad \alpha_v = 0.60$$

$$\text{design shear resistance total: } V_{Rd,1} = 222.2 \text{ kN}$$

angle leg 1 with bearing resistance:

$$\text{design bearing resistance total: } V_{Rd,2} = 1152.2 \text{ kN}$$

angle leg 1 with shear (gross section):

$$\text{shear resistance } V_{Rd} = (A_v \cdot f_y) / (3^{1/2} \cdot \gamma_{M0}) = 298.49 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,3} = 2 \cdot V_{Rd} / 1.27 = 470.1 \text{ kN}$$

angle leg 1 with shear (net section):

$$\text{shear resistance } V_{Rd} = (A_{v,net} \cdot f_u) / (3^{1/2} \cdot \gamma_{M2}) = 256.07 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,4} = 2 \cdot V_{Rd} = 512.1 \text{ kN}$$

angle leg 1 in tension and shear (shear block):

$$\text{shear resistance } V_{eff,Rd} = (0.5 \cdot A_{nt} \cdot f_u) / \gamma_{M2} + (A_{nv} \cdot f_y / 3^{1/2}) / \gamma_{M0} = 211.36 \text{ kN}$$

$$\text{shear resistance total: } V_{Rd,5} = 2 \cdot V_{eff,Rd} = 422.7 \text{ kN}$$

angle leg 1 in bending and shear:

$$b_F = 220.0 \text{ mm} > 2.73 \cdot z = 163.8 \text{ mm:}$$

shear resistance total:  $V_{Rd,6} = \infty$

angle leg 1 with buckling:

$z_F = 60.0 \text{ mm} < t_F/0.15 = 66.7 \text{ mm}$ :

shear resistance total:  $V_{Rd,7} = \infty$

beam web (sb) with bearing resistance:

design bearing resistance total:  $V_{Rd,8} = 238.3 \text{ kN}$

beam web (sb) with shear (gross section):

shear resistance  $V_{Rd} = (A_v \cdot f_y) / (3^{1/2} \cdot \gamma_{M0}) = 348.44 \text{ kN}$

shear resistance total:  $V_{Rd,9} = 348.4 \text{ kN}$

beam web (sb) with shear (net section):

shear resistance  $V_{Rd} = (A_{v,net} \cdot f_u) / (3^{1/2} \cdot \gamma_{M2}) = 349.11 \text{ kN}$

shear resistance total:  $V_{Rd,10} = 349.1 \text{ kN}$

beam web (sb) in tension and shear (shear block):

shear resistance  $V_{eff,Rd} = (0.5 \cdot A_{nt} \cdot f_u) / \gamma_{M2} + (A_{nv} \cdot f_y / 3^{1/2}) / \gamma_{M0} = 198.82 \text{ kN}$

shear resistance total:  $V_{Rd,11} = 198.8 \text{ kN}$

**shear resistance: min  $V_{Rd,a1} = V_{Rd,11} = 198.8 \text{ kN}$**

**design resistance: min  $V_{Rd} = 198.8 \text{ kN}$**

**required plate thickness of main girder web:**

beam web (mg) with bearing resistance:

design bearing resistance:  $V_{Rd} = 198.8 \text{ kN}$

erf  $t_u = \min V_{Rd} \cdot t / V_{Rd} = 3.30 \text{ mm}$

## verification of the connection

$V_{Ed} = 89.7 \text{ kN}$ :  $V_{Ed} / \min V_{Rd} = 0.451 < 1$  **ok.**

### verification result

maximum utilization:  $\max U = 0.451 < 1$  **ok.**

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## Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe Dezember 2010

DIN EN 1993-1-8, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-8: Bemessung von Anschlüssen;

Deutsche Fassung EN 1993-1-8:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-8/NA, Nationaler Anhang zur DIN EN 1993-1-8, Ausgabe Dezember 2010

ECCS Document No. 126: European Recommendations for the Design of Simple Joints in Steel Structures.

ECCS TC10 - Structural Connections, 2009. J.P. Jaspart, J.F. Démonceau, S. Renkin, M.L. Guillaume

Klaus Weynand, Ralf Oerder: Typisierte Anschlüsse im Stahlhochbau nach DIN EN 1993-1-8,

IS - Gelenkige Stirnplattenanschlüsse, IW - Gelenkige Winkelanschlüsse

IG - Gelenkige Winkelanschlüsse mit großem Spalt, IK - Ausklinkungen,

Stahlbau Verlags- und Service GmbH, Ausgabe 2013