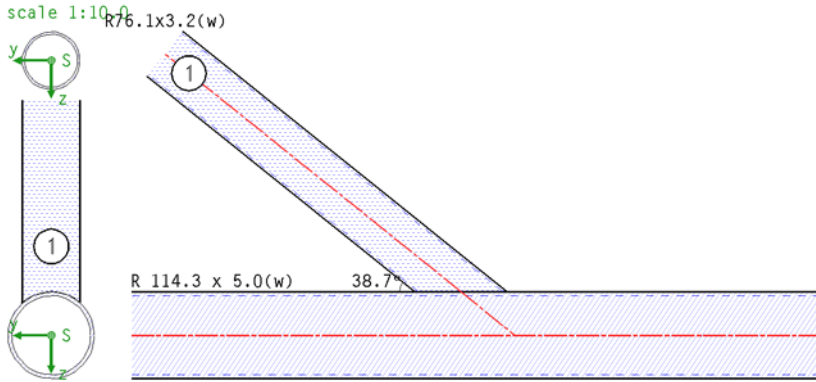


1. input report



steel

steel grade S235

material safety factor

resistance of cross-sections  $\gamma_{M0} = 1.00$

resistance of bolts, welds, plates in bearing  $\gamma_{M2} = 1.25$

resistance of hollow section joints  $\gamma_{M5} = 1.00$

geometry

T/Y joint

chord: section R 114.3 x 5.0(w)

brace 1: connection angle  $\Theta = 38.70^\circ$ , section R 76.1 x 3.2(w)

welds

fillet weld, weld thickness  $a = 3.2$  mm

verifications

verification of hollow section joint (chord and brace)

verification of welds with the directional method

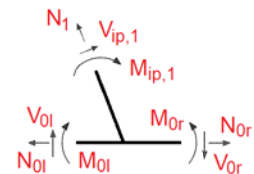
plastic verification of joining sections

internal forces and moments

Lk 1:  $N_{0l,Ed} = 97.00$  kN,  $N_{1,Ed} = -124.30$  kN

note

equilibrium is not checked.



check of data

brace 1:  $a = 3.2$  mm > req  $a = \beta_w \cdot 2^{1/2} \cdot f_y / f_u \cdot \gamma_{M2} / \gamma_{M0} \cdot t = 0.923 \cdot t_1 = 2.95$  mm **ok** (s. EC 3-1-8, 4.9(6))

brace 1: hollow section: plate thickness  $t_1 = 5.0$  mm > 2.5 mm **ok**

brace 1: hollow section: plate thickness  $t_2 = 3.2$  mm > 2.5 mm **ok**

brace 1: NA-DE: plate thickness  $t_{max} \geq 3$  mm: weld thickness  $a = 3.2$  mm >  $a_{min} = t_{max}^{1/2} - 0.5 = 1.74$  mm **ok**

brace 1: weld thickness  $a = 3.2$  mm >  $a_{min} = 3$  mm **ok**

coefficient  $\beta = d_1/d_0 = 0.666$

2. Lk 1

2.1. verification of a welded hollow section joint

design values:  $N_{1,Ed} = -124.30$  kN

range of validity (table 7.1, T/Y joint)

chord:  $10 < d_0/t_0 = 22.860 < 50$  **ok**

brace 1:  $0.2 < d_1/d_0 = 0.666 < 1$  **ok**

brace 1: section class 1 < 2 **ok**

resistance (table 7.2, T/Y joint)

coefficient  $\gamma = d_0/(2 \cdot t_0) = 11.430$

chord-preload force  $N_p = N_{0,Ed} - \sum(N_{i,Ed} \cdot \cos(\Theta_i)) = 97.0$  kN  $\Rightarrow$  coefficient  $k_p = 1$

brace 1:

chord face failure

resistance:  $N_{1,Rd} = (\gamma^{0.2} \cdot k_p \cdot f_y \cdot t_0^2) / \sin(\Theta_1) \cdot (2.8 + 14.2 \cdot \beta^2) / \gamma_{M5} = 139.11$  kN

utilisation:  $U_1 = N_{1,Ed} / N_{1,Rd} = 0.894 < 1$  **ok**

punching shear failure for  $d_1 = 76.1$  mm  $\leq d_0 - 2 \cdot t_0 = 104.3$  mm

resistance:  $N_{1,Rd} = f_y \cdot 0.3^{1/2} \cdot t_0 \cdot \pi \cdot d_1 \cdot (1 + \sin(\Theta_1)) / (2 \cdot \sin^2(\Theta_1)) / \gamma_{M5} = 337.13$  kN

utilisation:  $U_1 = N_{1,Ed} / N_{1,Rd} = 0.369 < 1$  **ok**

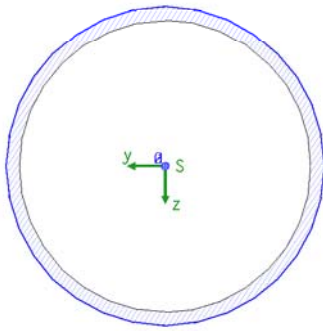
total:  $U_{Lk1} = 0.894 < 1$  **ok**

## 2.2. weld verification

### brace 1:

to simplify, the weld of a non-sloped or cut-out brace is verified

calculation section:



weld 1:  $a_w = 3.2 \text{ mm}$   $l_w = 239.1 \text{ mm}$

design values referring to centroid of the section:

$N_{Ed} = -124.30 \text{ kN}$

cross-sectional properties referring to centroid of the line cross-section:

$\Sigma A_w = 7.65 \text{ cm}^2$ ,  $A_{w,y} = 3.83 \text{ cm}^2$ ,  $A_{w,z} = 3.83 \text{ cm}^2$ ,  $\Sigma l_w = 23.9 \text{ cm}$

$I_{w,y} = 55.38 \text{ cm}^4$ ,  $I_{w,z} = 55.38 \text{ cm}^4$ ,  $\Delta y_w = 0.0 \text{ mm}$ ,  $\Delta z_w = 0.0 \text{ mm}$

verification of line section:

pt. 0:  $\sigma_{w,x} = -162.48 \text{ N/mm}^2$   $\tau_{w,t} = 0.00 \text{ N/mm}^2$   $\Rightarrow U_w = 0.591 < 1$  ok

pt. 1:  $\sigma_{w,x} = -162.48 \text{ N/mm}^2$   $\tau_{w,t} = 0.00 \text{ N/mm}^2$   $\Rightarrow U_w = 0.591 < 1$  ok

pt. 2:  $\sigma_{w,x} = -162.48 \text{ N/mm}^2$   $\tau_{w,t} = 0.00 \text{ N/mm}^2$   $\Rightarrow U_w = 0.591 < 1$  ok

pt. 3:  $\sigma_{w,x} = -162.48 \text{ N/mm}^2$   $\tau_{w,t} = 0.00 \text{ N/mm}^2$   $\Rightarrow U_w = 0.591 < 1$  ok

Result:

pt. 0:  $\sigma_{w,x} = -162.48 \text{ N/mm}^2$   $\tau_{w,t} = 0.00 \text{ N/mm}^2$

Max:  $\sigma_{1,w,Ed} = 17.94 \text{ kN/cm}^2 < f_{1w,d} = 36.00 \text{ kN/cm}^2$ ,

$\sigma_{2,w,Ed} = 15.33 \text{ kN/cm}^2 < f_{2w,d} = 25.92 \text{ kN/cm}^2 \Rightarrow U_w = 0.591 < 1$  ok

## 2.3. verification of cross-section

chord:

plastic verification for  $N = 97.00 \text{ kN}$

plastic values:  $N_{pl,Rd} = A \cdot f_y / \gamma_{M0} = 403.47 \text{ kN}$

verification:  $|N_{Ed}| / N_{pl,Rd} = 0.240 < 1$  ok

brace 1:

plastic verification for  $N = -124.30 \text{ kN}$

plastic values:  $N_{pl,Rd} = A \cdot f_y / \gamma_{M0} = 172.22 \text{ kN}$

verification:  $|N_{Ed}| / N_{pl,Rd} = 0.722 < 1$  ok

## 2.4. check of the hinge rotation (EC 3-1-8, 4.9(6))

brace 1:  $U_w = 0.591 < U = 0.894$  ok

## 3. final result

maximum utilisation: resistance max  $U = 0.894 < 1$  ok

verification succeeded

## 4. Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;

Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010

DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;

Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010

DIN EN 1993-1-1/A1, Ergänzungen zur DIN EN 1993-1-1, Ausgabe Juli 2014

DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe Dezember 2018

DIN EN 1993-1-8, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -

Teil 1-8: Bemessung von Anschlüssen;

Deutsche Fassung EN 1993-1-8:2005 + AC:2009, Ausgabe Dezember 2010

