

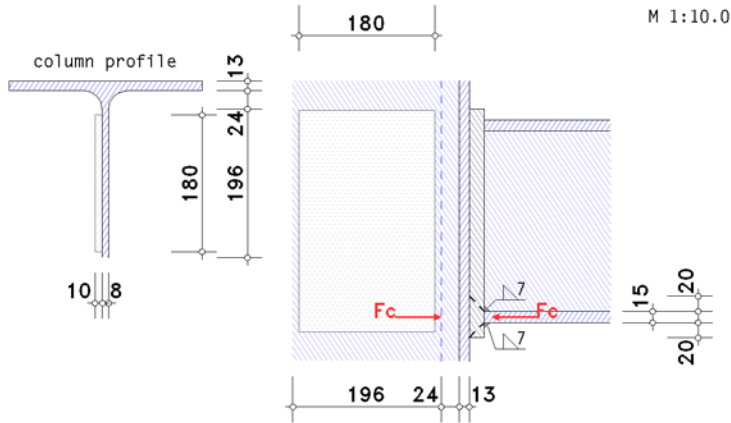
POS. 24: COLUMN WEB IN TRANSVERSE COMPRESSION

4H-EC3GK version: 1/2012-1k

beam or column web in transverse compression

Basic component 2

EC 3-1-8 (12.10), NA: Germany



column:

- clear depth of the web $d_c = 196.0$ mm
- web thickness $t_{wc} = 8.0$ mm
- flange thickness $t_{fc} = 13.0$ mm
- root resp. leg length of the web weld $s_c = 24.0$ mm
- steel grade S 275
- shear area (without reinforcement) $A_{vc} = 3174.00$ mm²

beam:

- flange thickness $t_{fb} = 15.0$ mm
- weld between beam compression flange and end-plate: $a_p = 7.0$ mm
- dispersion measure through end-plate: $s_p = 2 \cdot 20.0 = 40.0$ mm
- reinforcement of column web with 1 supplementary web plate(s):
 - plate thickness $t_s = 10.0$ mm, width $b_s = 180.0$ mm
- longitudinal compressive stress in column web $\sigma_{com,Ed} = 159.0$ N/mm²
- transformation parameter $\beta = 1.00$
- safety factors: $\gamma_{M0} = 1.00$, $\gamma_{M1} = 1.10$

stress:

- Lk 1 : $F_{c,wc,Ed} = 300.0$ kN

design resistance

- thickness of supplementary web plate $t_s = 10.0$ mm > thickness of column web $t_{wc} = 8.0$ mm **ok**.
- width of supplementary web plate $b_s = 180.0$ mm < clear depth of the column web $d_c = 196.0$ mm **ok**.
- width of supplementary web plate $b_s = 180.0$ mm < $40 \cdot \varepsilon \cdot t_s = 369.77$ mm, $\varepsilon = 0.92$ **ok**.
- width of supplementary web plate $b_s = 180.0$ mm > $d_c - 2 \cdot t_s = 176.0$ mm, ass.: fillet weld with $a_s = t_s / 2^{0.5} = 7.1$ mm **ok**.

effective width of column web in transverse compression $b_{eff,c,wc} = t_{fb} + 2 \cdot 2^{1/2} \cdot a_p + 5 \cdot (t_{fc} + s_c) + s_p = 259.8$ mm

reinforcement of web with 1 supplementary web plate: effective web thickness $t_w = (1 + 0.5 \cdot n_s \cdot t_w) = 12.0$ mm

assembly of supplementary web plates:

- increase of shear area of $b_s \cdot t_s, eff = 720.00$ mm², $t_{s,eff} = 4.0$ mm
- shear area with supplementary web plates $A_v = 3894.00$ mm²
- plate slenderness $\lambda_p = 0.932 \cdot [(b_{eff,c} \cdot d_w \cdot f_y) / (E \cdot t_w^2)]^{1/2} = 0.634$
- reduction factor for web buckling $\rho = (\lambda_p - 0.2) / \lambda_p^2 = 1.08 > 1.0 \Rightarrow \rho = 1.00$
- reduction factor for interaction with shear stress: $\beta = 1 \Rightarrow \omega = 0.74$

design resistance of column/beam web in transverse compression:

$$F_{c,w,Rd} = \omega \cdot (k_w \cdot b_{eff,c} \cdot t_w \cdot f_{y,w}) / \gamma_{M0} = 633.2 \text{ kN}, \quad k_w = 1.00$$

$$F_{c,w,Rd,max} = \omega \cdot (k_w \cdot \rho \cdot b_{eff,c} \cdot t_w \cdot f_{y,w}) / \gamma_{M1} = 575.6 \text{ kN}$$

$$F_{c,w,Rd} > F_{c,w,Rd,max} \Rightarrow F_{c,w,Rd} = 575.6 \text{ kN}$$

verification

Lk 1: $F_{Ed} = 300.0 \text{ kN} < F_{Rd} = 575.6 \text{ kN} \Rightarrow \text{utilization} = 0.521 < 1$ **ok.**