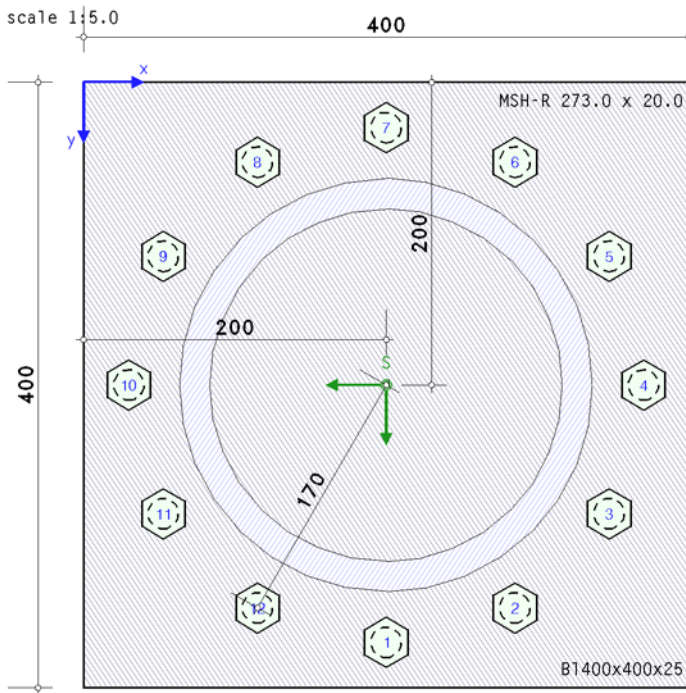


**bolted end-plate connection**

EC 3-1-8 (12.10), NA: Deutschland



**steel grade**

steel grade S235

**bolts**

bolt class 10.9, bolt size M20, thread included in the shear plane

**connection**

end-plate: thickness  $t_p = 25.0$  mm, width  $b_p = 400.0$  mm, length  $l_p = 400.0$  mm

beam: section MSH-R 273.0 x 20.0

beam-end-plate: surrounding butt weld (full penetrated)

beam section centric on end-plate (coinciding centroids)

coordinates of beam centroid on end-plate  $x_s = 200.0$  mm,  $y_s = 200.0$  mm

bolts:

circular arrangement of 12 bolts with radius  $r = 170.0$  mm around centroid of beam section

**calculation**

verification:

calculation and verification of internal forces and moments (FEM)

verification of end-plate with the plastic method

verification of beam section with the plastic method

verification of welds with the directional method

verification of bolts, check of distances

FEM-calculation:

bolts are plastically calculated, spring constant of bolts  $c_f = 9596.1$  kN/cm

plastic limit force  $F_{t,f} = f_{t,f} \cdot F_{t,Rd} = 167.6$  kN,  $f_{t,f} = 0.950$ ,  $F_{t,Rd} = 176.4$  kN, effective elongation at failure  $\epsilon_{t,f} = 4.5\%$  without preloading ( $F_p, c = 0$ )

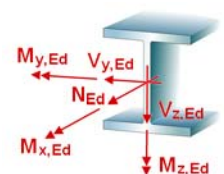
effective foundation modulus of end plate  $c_b = 16800.0$  kN/cm<sup>3</sup>

number / dimension of finite elements each direction  $n_x / \Delta x = 20 / 20.0$  mm,  $n_y / \Delta y = 20 / 20.0$  mm

max. 50 iteration steps (tolerance limit 5‰)

**internal forces and moments**

Lk	$N_{Ed}$ kN	$M_{y,Ed}$ kNm	$V_{z,Ed}$ kN	$M_{z,Ed}$ kNm	$V_{y,Ed}$ kN	$M_{x,Ed}$ kNm
1	-169.4	-183.9	-36.8	91.7	-18.3	50.1
2	60.3	22.7	4.5	-184.5	18.1	-83.6
3	-143.3	-138.7	-27.7	127.8	-25.6	63.4
4	23.4	-40.9	-8.2	-182.8	17.8	-87.4
5	-106.4	-75.1	-15.0	126.1	-25.2	67.2
6	-168.1	-175.7	-35.1	89.6	-17.9	54.8
7	59.4	17.0	3.4	-183.0	17.9	-86.9



**partial safety factors for material**

resistance of cross-sections  $\gamma_{M0} = 1.00$

## Calculation

### utilizations

Lk	$U_p$	$U_\sigma$	$U_b$	$U_{wt}$	$U_{t,s}$	$U_{vt,s}$	$U_{b,s}$	$U_q$	$U_{c/t}$	$U_w$	U
1	0.694	0.694	0.335	0.264	0.950	0.714	0.149	0.718	0.195	0.736	0.950*
2	0.731	0.731	0.288	0.262	0.950	0.921	0.293	0.696	0.115	0.660	0.950*
3	0.649	0.649	0.314	0.194	0.941	0.728	0.181	0.680	0.126	0.678	0.941
4	0.718	0.718	0.294	0.244	0.950	0.912	0.325	0.707	0.117	0.659	0.950*
5	0.458	0.458	0.237	0.133	0.800	0.698	0.168	0.557	0.097	0.535	0.800
6	0.648	0.648	0.321	0.226	0.950	0.714	0.154	0.697	0.132	0.709	0.950*
7	0.727	0.727	0.286	0.245	0.950	0.935	0.296	0.695	0.114	0.655	0.950*

$U_p$ : utilization of end-plate;  $U_\sigma$ : utilization of end-plate due to stress;  $U_b$ : utilization of end-plate due to compression by contact  
 $U_{wt,s}$ : utilization of bolts due to elongation;  $U_{t,s}$ : utilization of bolts due to tension;  $U_{vt,s}$ : utilization of bolts due to shear in tension  
 $U_{b,s}$ : utilization of bolts due to bearing resistance;  $U_q$ : stress utilization of beam;  $U_{c/t}$ : c/t-utilization of beam  
 $U_w$ : utilization of welds; U: total utilization  
 \*) maximum utilization

## Final Result

maximum utilization [Lk 1] max U = 0.950 < 1 ok.

verification succeeded

## Regulations

DIN EN 1990, Eurocode 0: Grundlagen der Tragwerksplanung;  
 Deutsche Fassung EN 1990:2002 + A1:2005 + A1:2005/AC:2010, Ausgabe Dezember 2010  
 DIN EN 1990/NA, Nationaler Anhang zur DIN EN 1990, Ausgabe Dezember 2010

DIN EN 1993-1-1, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -  
 Teil 1-1: Allgemeine Bemessungsregeln und Regeln für den Hochbau;  
 Deutsche Fassung EN 1993-1-1:2005 + AC:2009, Ausgabe Dezember 2010  
 DIN EN 1993-1-1/NA, Nationaler Anhang zur DIN EN 1993-1-1, Ausgabe Dezember 2010

DIN EN 1993-1-8, Eurocode 3: Bemessung und Konstruktion von Stahlbauten -  
 Teil 1-8: Bemessung von Anschlüssen;  
 Deutsche Fassung EN 1993-1-8:2005 + AC:2009, Ausgabe Dezember 2010  
 DIN EN 1993-1-8/NA, Nationaler Anhang zur DIN EN 1993-1-8, Ausgabe Dezember 2010

## Detailed edition of Lk 1 (decisive)

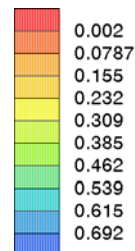
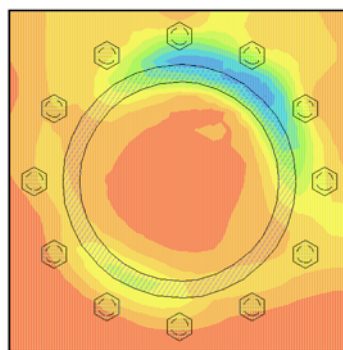
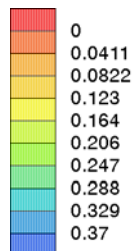
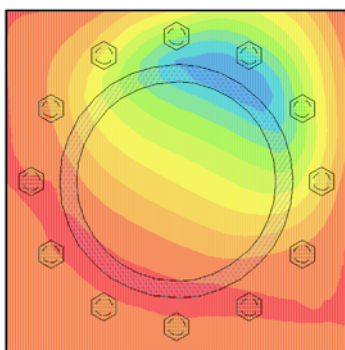
Lk 1:  $N_{Ed} = -169.4$  kN,  $M_{y,Ed} = -183.9$  kNm,  $V_{z,Ed} = -36.8$  kN,  $M_{z,Ed} = 91.7$  kNm, V

### end-plate

design values:  $N = -169.42$  kN,  $M_y = -183.86$  kNm,  $M_z = 91.74$  kNm

deformations  $u_z$  [mm], lifting off positive  
 min  $u_z = -0.01$  mm, max  $u_z = 0.37$  mm

utilization of end-plate  $U_p$   
 min  $U_p = 0.002$ , max  $U_p = 0.694$



## utilization of end-plate

Kno	x mm	y mm	u <sub>z</sub> mm	U <sub>σ</sub>	U <sub>b</sub>	U <sub>p</sub>
278	260.0	80.0	0.370	0.656	---	0.656
321	300.0	100.0	0.360	0.694	---	0.694

x,y: node coordinates; u<sub>z</sub>: deformations (lifting off positive); U<sub>σ</sub>: utilization due to moment with shear force; U<sub>b</sub>: utilization due to compression by contact  
U<sub>p</sub>: utilization of end-plate

## tension force of bolts

	x mm	y mm	w <sub>t</sub> mm	F <sub>t</sub> kN	ε <sub>w<sub>t</sub></sub> %	U <sub>w<sub>t</sub></sub>
1	200.0	370.0	0.005	4.63	0.018	0.004
2	285.0	347.2	-0.001	0.15	---	---
3	347.2	285.0	0.028	27.12	0.113	0.025
4	370.0	200.0	0.100	95.38	0.398	0.089
5	347.2	115.0	0.219	165.53	0.874	0.194
6	285.0	52.8	0.298	167.58	1.190	0.264
7	200.0	30.0	0.234	166.36	0.935	0.208
8	115.0	52.8	0.131	123.92	0.524	0.117
9	52.8	115.0	0.044	42.42	0.177	0.039
10	30.0	200.0	-0.000	0.46	---	---
11	52.8	285.0	0.002	2.75	0.008	0.002
12	115.0	347.2	0.006	5.74	0.022	0.005

x,y: bolt coordinates; w<sub>t</sub>: deformation (tension positive); F<sub>t</sub>: bolt force; ε<sub>w<sub>t</sub></sub>: elongation  
U<sub>w<sub>t</sub></sub>: utilization due to elongation

utilization of end-plate [node 321] U<sub>max</sub> = 0.694 < 1 **ok.**

utilization of bolts due to elongation [bolt 6] U<sub>max</sub> = 0.264 < 1 **ok.**

## bolts

design values: max F<sub>t</sub> = 167.58 kN, V<sub>z</sub> = -36.77 kN, V<sub>y</sub> = -18.35 kN, M<sub>x</sub> = 50.10 kNm

## verification of bolts

U<sub>tp</sub> utilization due to tension/punching shear failure, U<sub>vt</sub> utilization due to shear in tension, U<sub>b</sub> utilization due to bearing resistance, U utilization of bolts

bolt 1	U <sub>tp,1</sub> = 0.026	U <sub>vt,1</sub> = 0.368	U <sub>b,1</sub> = 0.132	U <sub>1</sub> = 0.368
bolt 2	U <sub>tp,2</sub> = 0.001	U <sub>vt,2</sub> = 0.000	U <sub>b,2</sub> = 0.149	U <sub>2</sub> = 0.467
bolt 3	U <sub>tp,3</sub> = 0.154	U <sub>vt,3</sub> = 0.593	U <sub>b,3</sub> = 0.132	U <sub>3</sub> = 0.593
bolt 4	U <sub>tp,4</sub> = 0.541	U <sub>vt,4</sub> = 0.685	U <sub>b,4</sub> = 0.103	U <sub>4</sub> = 0.685
bolt 5	U <sub>tp,5</sub> = 0.938	U <sub>vt,5</sub> = 0.713	U <sub>b,5</sub> = 0.013	U <sub>5</sub> = 0.938
bolt 6	U <sub>tp,6</sub> = 0.950	U <sub>vt,6</sub> = 0.714	U <sub>b,6</sub> = 0.010	U <sub>6</sub> = 0.950
bolt 7	U <sub>tp,7</sub> = 0.943	U <sub>vt,7</sub> = 0.712	U <sub>b,7</sub> = 0.013	U <sub>7</sub> = 0.943
bolt 8	U <sub>tp,8</sub> = 0.702	U <sub>vt,8</sub> = 0.679	U <sub>b,8</sub> = 0.049	U <sub>8</sub> = 0.702
bolt 9	U <sub>tp,9</sub> = 0.240	U <sub>vt,9</sub> = 0.548	U <sub>b,9</sub> = 0.120	U <sub>9</sub> = 0.548
bolt 10	U <sub>tp,10</sub> = 0.003	U <sub>vt,10</sub> = 0.386	U <sub>b,10</sub> = 0.148	U <sub>10</sub> = 0.386
bolt 11	U <sub>tp,11</sub> = 0.016	U <sub>vt,11</sub> = 0.303	U <sub>b,11</sub> = 0.081	U <sub>11</sub> = 0.303
bolt 12	U <sub>tp,12</sub> = 0.033	U <sub>vt,12</sub> = 0.298	U <sub>b,12</sub> = 0.078	U <sub>12</sub> = 0.298
total Max:	U <sub>tp</sub> = 0.950	U <sub>vt</sub> = 0.714	U <sub>b</sub> = 0.149	U = 0.950 < 1 <b>ok.</b>

utilization of bolts [bolt 6] U<sub>max</sub> = 0.950 < 1 **ok.**

## beam

plastic cross-sectional check for N = -169.42 kN, M<sub>y</sub> = -183.86 kNm, V<sub>z</sub> = -36.77 kN,

M<sub>z</sub> = 91.74 kNm, V<sub>y</sub> = -18.35 kN, M<sub>x</sub> = 50.10 kNm

valid normal-/shear stress: zul σ<sub>Rd</sub> = 23.50 kN/cm<sup>2</sup>, zul τ<sub>Rd</sub> = 13.57 kN/cm<sup>2</sup>

web: shear force V<sub>s</sub> = 41.10 kN, torsion T<sub>ps</sub> = 50.10 kNm, shear stress τ<sub>s</sub> = 2.89 kN/cm<sup>2</sup> ⇒ U<sub>τ,s</sub> = 0.213

design resistance forces N<sub>max,s</sub> = 3649.79 kN, N<sub>min,s</sub> = -3649.79 kN

main bending: axial force N = -169.42 kN, design resistance forces N<sub>max</sub> = 3649.79 kN, N<sub>min</sub> = -3649.79 kN ⇒ U<sub>N</sub> = 0.046

moment M<sub>y</sub> = 205.48 kNm, design resistance moments M<sub>y,max</sub> = 293.76 kNm, M<sub>y,min</sub> = -293.76 kNm ⇒ U<sub>M<sub>y</sub></sub> = 0.69

total (possibly due to load increase): max U = 0.718 < 1 **ok.**

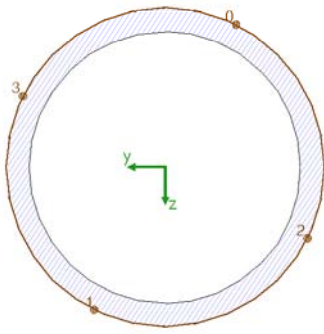
utilizations: design resistance U<sub>σ</sub> = 0.718 < 1 **ok.**, c/t-ratio U<sub>c/t</sub> = 0.195 < 1 **ok.**

utilization of beam max(U<sub>σ</sub>, U<sub>c/t</sub>) = 0.718 < 1 **ok.**

## welds

design values: N = -169.42 kN, M<sub>y</sub> = -183.86 kNm, V<sub>z</sub> = -36.77 kN, M<sub>z</sub> = 91.74 kNm,

V<sub>y</sub> = -18.35 kN, M<sub>x</sub> = 50.10 kNm



weld 1:  $a_w = 20.0 \text{ mm}$   $l_w = 857.7 \text{ mm}$

Max:  $\sigma_{1,w,Ed} = 26.48 \text{ kN/cm}^2 < f_{1,w,Rd} = 36.00 \text{ kN/cm}^2$ ,  
 $\sigma_{2,w,Ed} = 13.11 \text{ kN/cm}^2 < f_{2,w,Rd} = 25.92 \text{ kN/cm}^2 \Rightarrow U_w = 0.736 < 1$  **ok.**

utilization of welds  $U_{max} = 0.736 < 1$  **ok.**

utilization Lk 1  $U_{max} = 0.950 < 1$  **ok.**